

Cavitation Within Fuel Injectors: Development and Multiscale Validation of Euler-Lagrange based Computational Methods for Modeling Cavitation within Fuel Injectors

Project ID: ACS104

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Overview

Timeline

- Project start date: 2/01/2016
- Project end date: 1/31/2019
- Percent complete: 36%

Budget

- Total project funding
 - DOE share: \$543,074
 - Contractor share: \$200,000
- Funding received in FY 2016: \$180,989
- Funding for FY 2017: \$180,989

Barriers

- Barriers addressed
 - Lack of fundamental knowledge of advanced engine combustion regimes
 - Lack of modeling capability for combustion and emission control

Partners

- Boston University – Lead
- Oak Ridge National Laboratory

Objectives and Relevance

Overall Objective

- To develop and validate more accurate, physics-based, mathematical submodels for use in standard multiphase CFD software to enable better prediction of cavitation within fuel injectors.

Objectives this period

- Select appropriate open source Lagrangian code for cavitation simulations
- Construct small scale experimental setup of cavitation in a canonical nozzle
- Image cavitation in real fuel injector using the High Flux Isotope Reactor (HFIR) at Oak Ridge National Laboratory (ORNL).

Impact

- Computational models will allow more detailed studies of cavitation within fuel injectors
- Small scale experiments will provide insight into conditions causing cavitation
- Small scale experiments and HFIR data provide validation data to ensure accurate simulations

Milestones

| Milestone and Go/No-Go Decision Points | Planned Date |
|---|-------------------|
| Microscale experiments required for SPH development completed | August 30, 2017 |
| Second measurement campaign completed | November 30, 2017 |
| Significant population of cavitation database, so upscaling can begin. | June 30, 2017 |
| First results from upscaling obtained | August 30, 2017 |
| Go/No-Go: Simulation of bubble dynamics with the SPH method, as evidenced by initial validation results | January 31, 2018 |

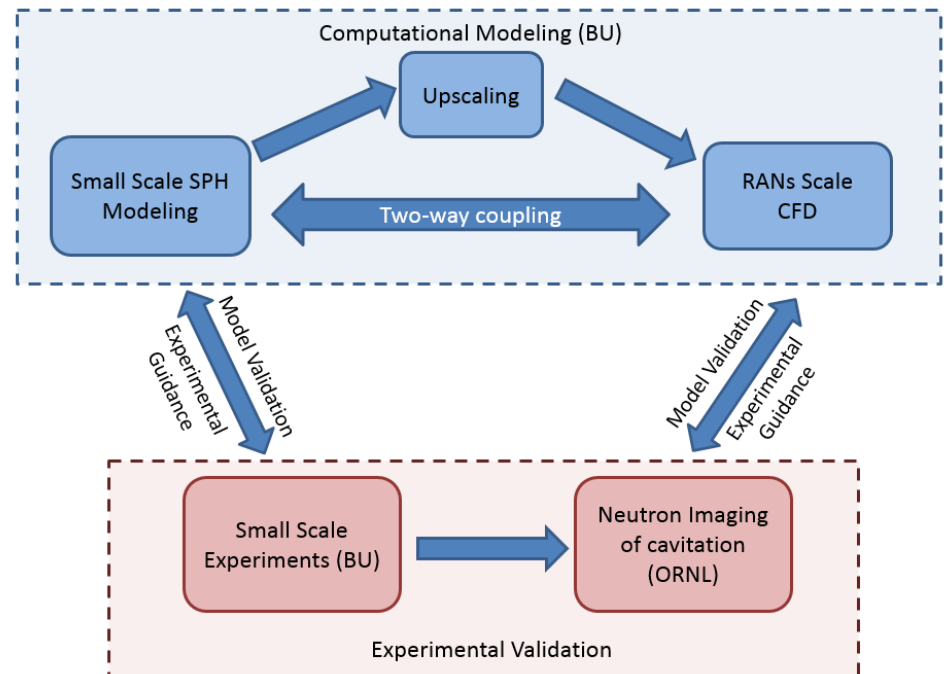
Technical Approach

Computational Development

- Lagrangian particle based model of bubble dynamics
- Coupling of Lagrangian model to RANS CFD

Experimental Characterization and Validation

- Small-scale experiments in idealized fuel injector
- Neutron imaging of cavitation in real fuel injector



Technical Accomplishments: Smoothed Particle Hydrodynamics Simulations of Multiphase Flow

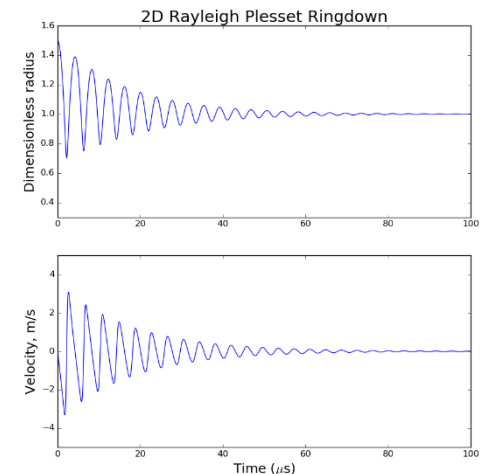
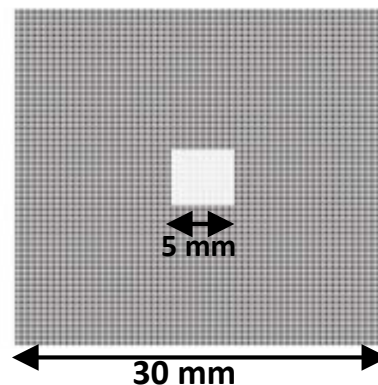
Goal: Simulate bubble behavior inside fuel injector nozzle

Initial work focuses on inclusion of appropriate sub-models for surface tension, pressure, etc. and validation of bubble dynamics

Validation cases:

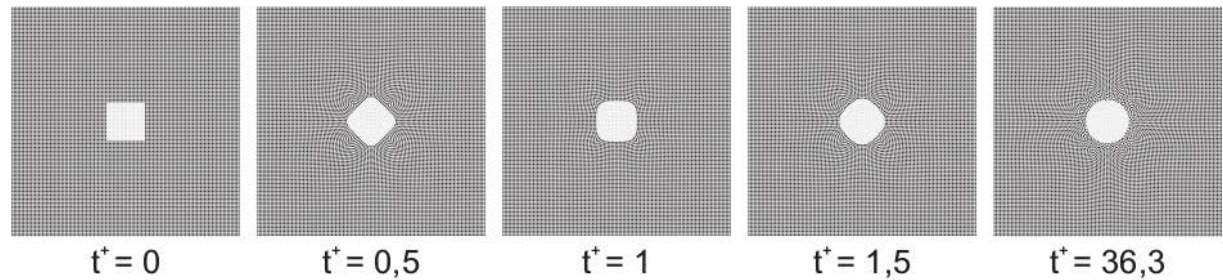
- Consider cases for air bubble in water or water droplet in air ($\rho_w/\rho_a = 1000$)
- Simulations of gas bubble and liquid droplet shape oscillations
- Rayleigh – Plesset solution for bubble dynamics

$$\tau = 2\pi\sqrt{\frac{\rho R^3}{\sigma(n^3 - n)}}$$

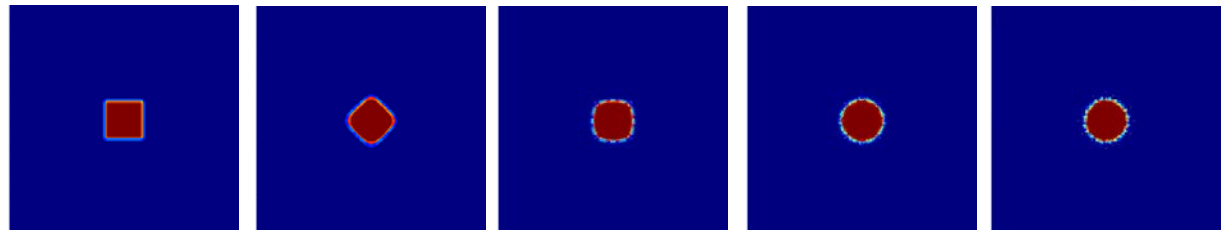


Technical Accomplishments: Liquid Droplet and Gas Bubble Shape Oscillations

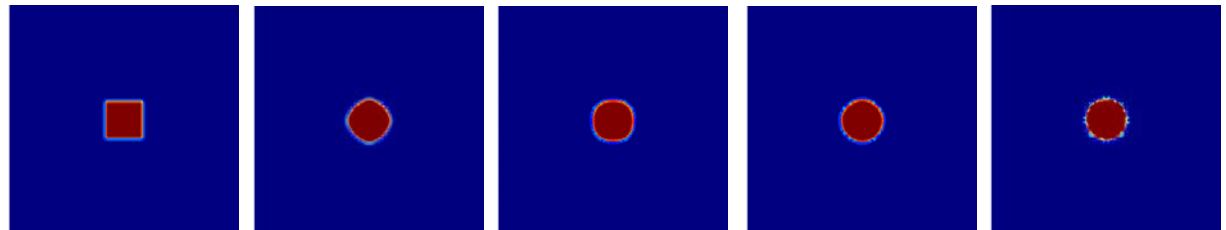
Liquid Droplet from Literature



Liquid Droplet



Gas Bubble



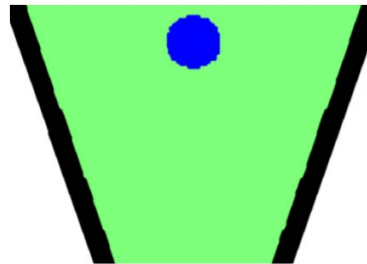
Technical Accomplishments: On Going SPH Bubble Modeling

Focusing on single bubble dynamics before moving to multiple bubbles

Incorporating bubble dynamics into nozzle simulation

Next steps inclusion of wall effects, multi bubble dynamics

Hua et al 2007



| Test Case | Experiments | | Simulation | |
|-----------|---|---------------------------------|----------------------------------|--|
| | Test conditions | Observed terminal bubble shapes | Predicted terminal bubble shapes | Modeling conditions |
| B1 | $E=116$ $Ma=48$ $Re=2.47$ | | | $Bo^*=116$ $Re^*=546$ $U^*=0.354$ |
| B2 | $E=116$ $Ma=266$ $Re=3.57$ | | | $Bo^*=116$ $Re^*=8.748$ $U^*=0.414$ |
| B3 | $E=116$ $Ma=11.1$ $Re=7.16$ | | | $Bo^*=116$ $Re^*=13.95$ $U^*=0.302$ |
| B4 | $E=116$ $Ma=5.51$ $Re=13.3$ | | | $Bo^*=116$ $Re^*=23.06$ $U^*=0.571$ |
| B5 | $E=116$ $Ma=1.31$ $Re=20.4$ | | | $Bo^*=116$ $Re^*=33.02$ $U^*=0.602$ |
| B6 | $E=116$ $Ma=0.103$ $Re=42.2$ | | | $Bo^*=116$ $Re^*=62.36$ $U^*=0.634$ |
| B7 | $E=116$ $Ma=6.5 \times 10^3$ $Re=8.0$ | | | $Bo^*=116$ $Re^*=15.4$ $U^*=0.600$ |
| B8 | $E=116$ $Ma=60 \times 10^3$ $Re=151$ | | | $Bo^*=116$ $Re^*=206.3$ $U^*=Unstable$ |

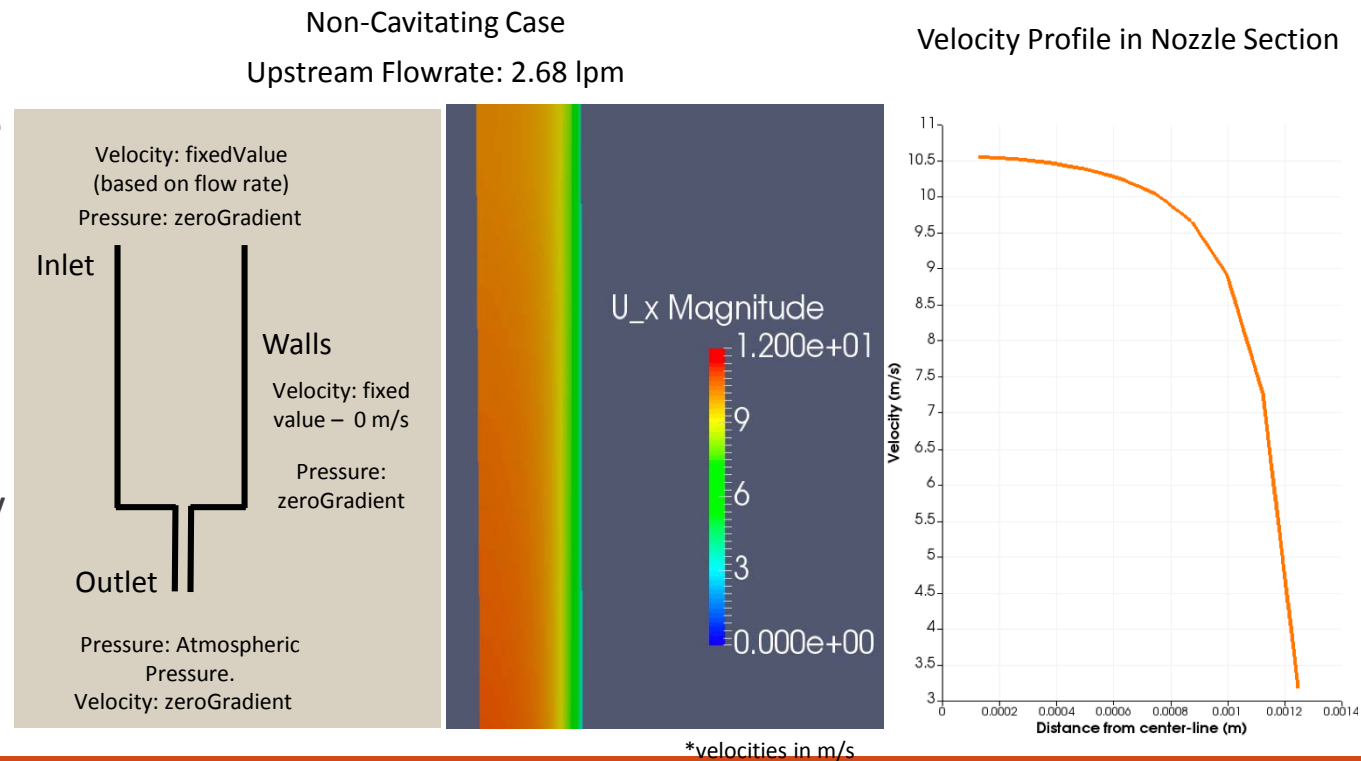
Technical Accomplishments: RANS Scale Simulations of Cavitation in a Nozzle

Goals:

- Investigate flow field in nozzle being tested at BU
- Gain better knowledge about current use of sub-models using homogenous volume fraction methods
- Utilize front tracking based volume of fluid (VOF) methods already in OpenFOAM

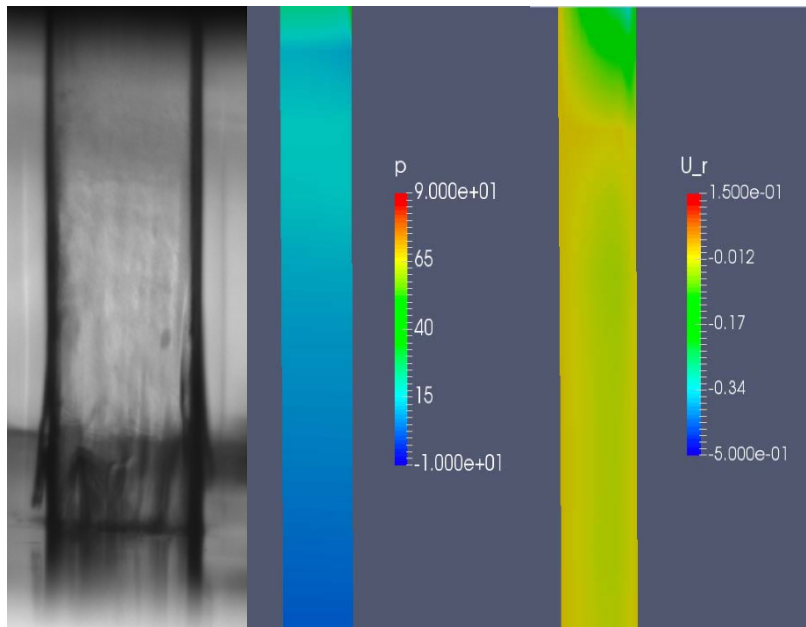
simpleFOAM:

steady state solver in OpenFOAM for incompressible flows with turbulence modelling. kEpsilon turbulence model used in simulations.



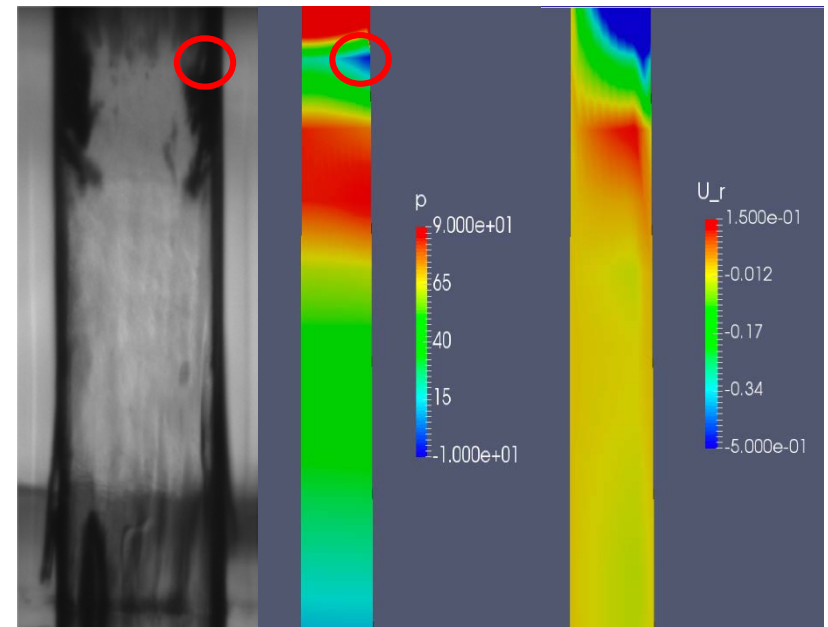
Technical Accomplishments: RANS CFD Results

Non-Cavitating Case



OpenFOAM simulations are shown from 0 to R
(model only half of experimental picture)

Cavitating Case



Low-Pressure is indication of cavitation in
simulations. Cavitation is also seen at a point
near the top of the nozzle in the
experiments

*velocities in m/s

Technical Accomplishments: Developed Acoustical Experimental Setup for Small Scale Experiments

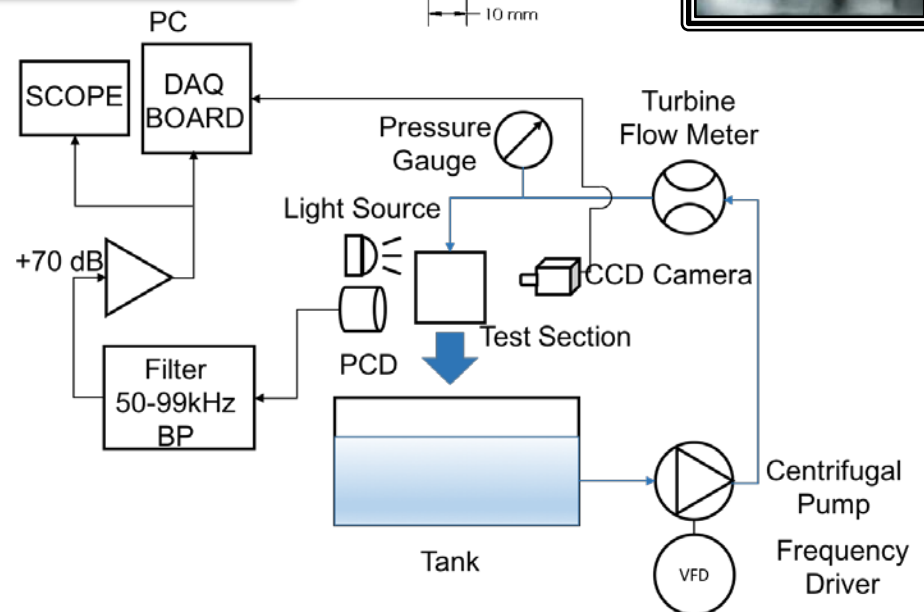
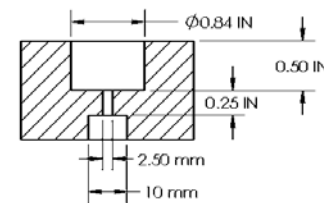
Conduct baseline flow cavitation experiments for comparison and validation of computations

- Acoustic diagnostic
- Optical diagnostic
- Flow variables:
 - Flow rate
 - Nozzle size
 - Nozzle geometry
- Material variables
 - Dissolved gas
 - Cavitation nuclei
 - Clean (Filtered 200nm)
 - Particulates
 - Microbubbles

Replaceable test section
with acoustic transducers



Example test section geometries

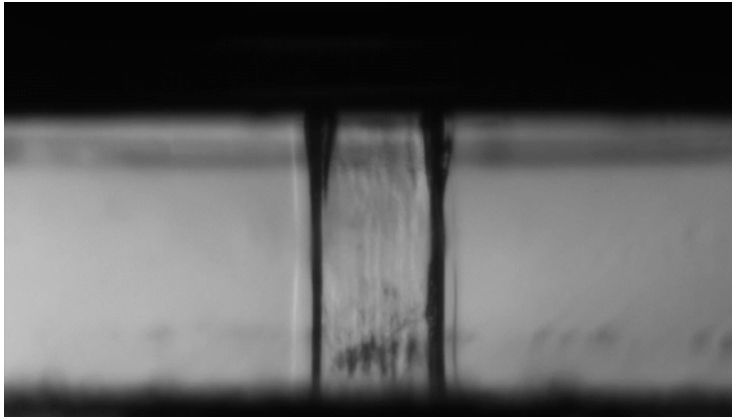


Technical Accomplishments: Stepped 2mm orifice results near onset

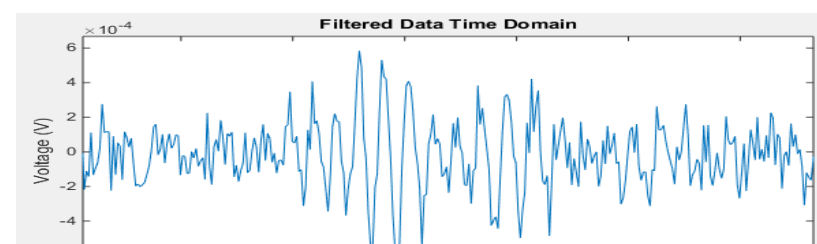
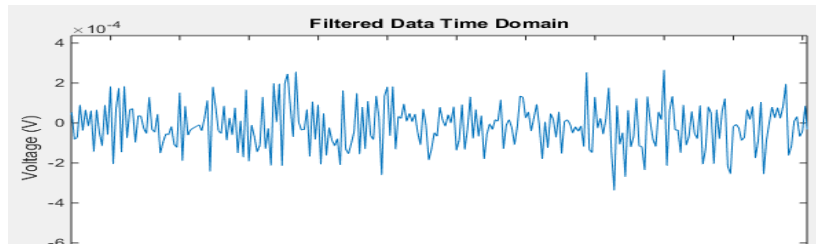
$Q = 43 \text{ mL/s}$ *No cavitation*

$Q = 68 \text{ mL/s}$ *Cavitation*

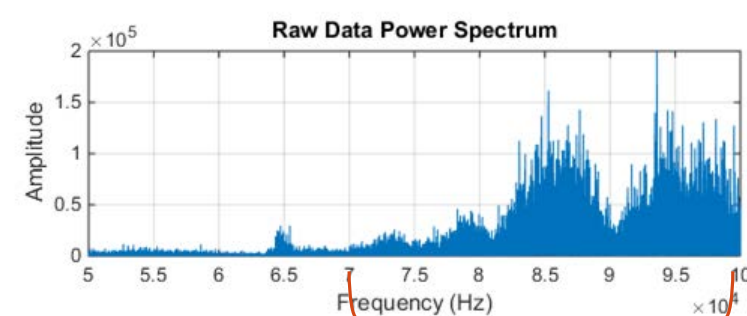
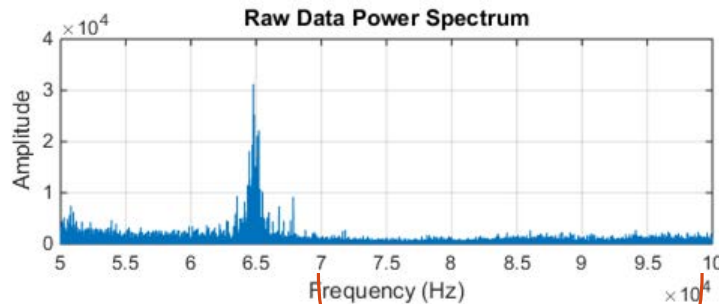
HS and
normal
imaging



Acoustic
time
series



Acoustic
spectral
domain



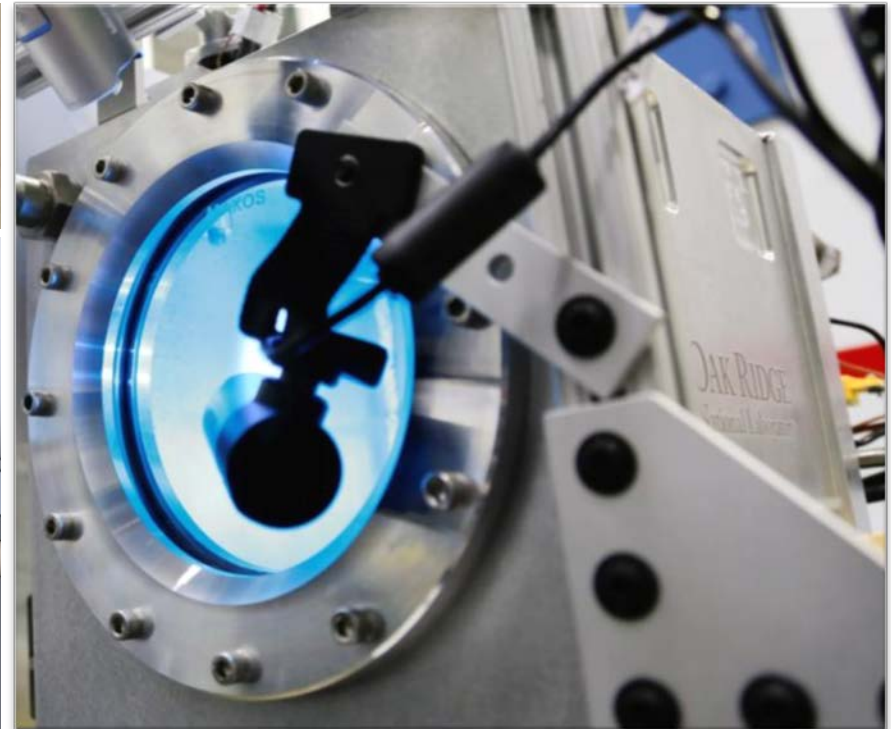
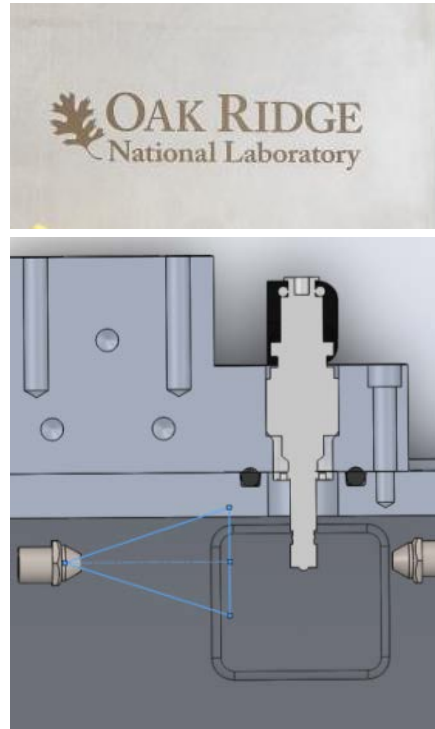
Detection band

Detection band

Technical Accomplishments: Imaging of fuel inject with ORNL High Flux Isotope Reactor (HFIR)

Spray chamber designed to allow for high sweep gas flow, sub-ambient P and elevated temperature

- Multiple cartridge heaters for fuel injector and chamber temperature control ($>100^{\circ}\text{C}$)
- Wide pressure range: 0.01 to 3-4 bar absolute (next generation target 6 bar)
- Direct heated sweep gas with high flowrate pumping system



Technical Accomplishments: Campaign performed at conditions to minimize fogging and encourage flash evaporation

Single hole injector from GM

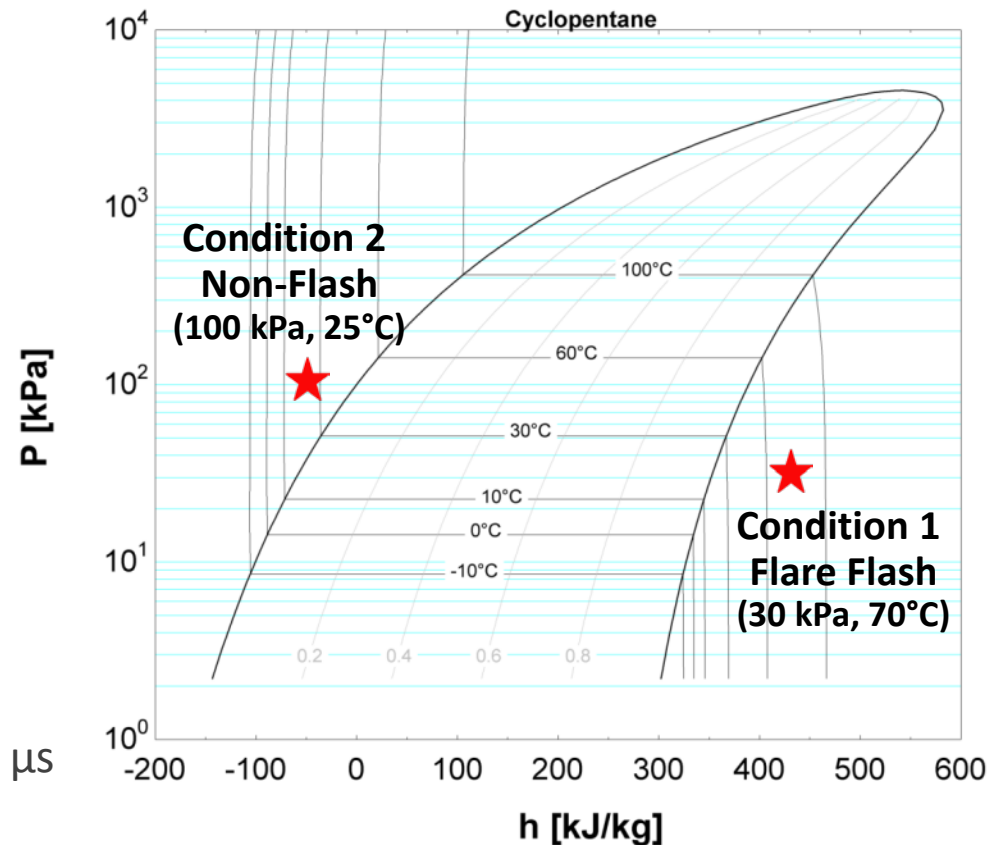
- Ron Grover and Scott Parrish

Fluid is cyclopentane

- Flash boils near ambient

Injection timing for composite image:

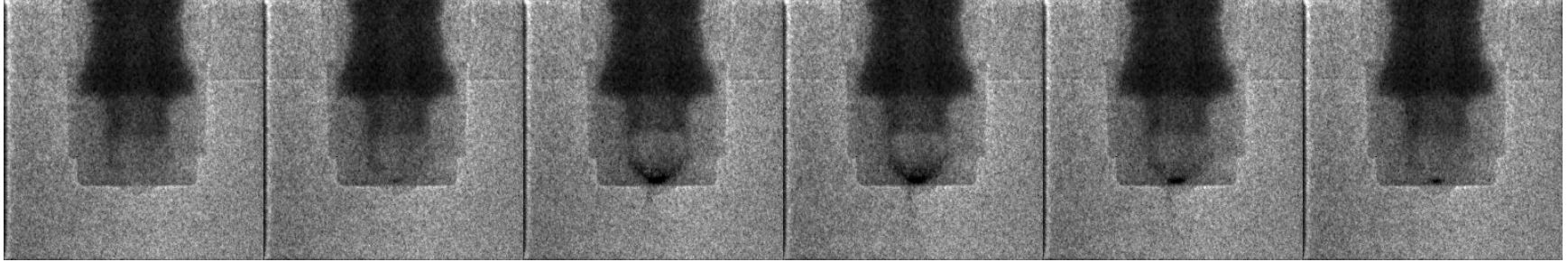
- 0.367 ms injection
- 25 Hz
- 20 μ s resolution
 - ~19 frames during injection
 - 1 ms before, ~5 ms after injection recorded
- ~40 s of neutron exposure for each 20 μ s frame over 20-24 hours
 - ~2M injections



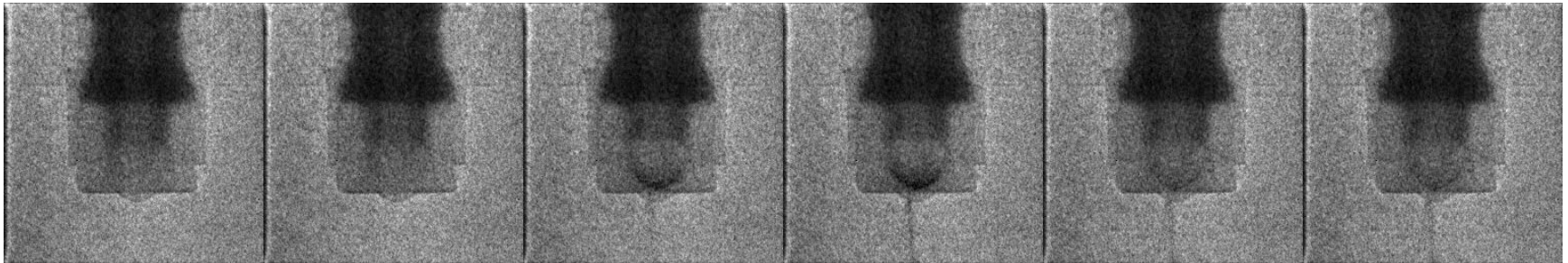
Technical Accomplishments:

Fluid behavior at the two conditions differ discernibly

Condition 1



Condition 2



1.28 ms

1.41 ms

1.54 ms

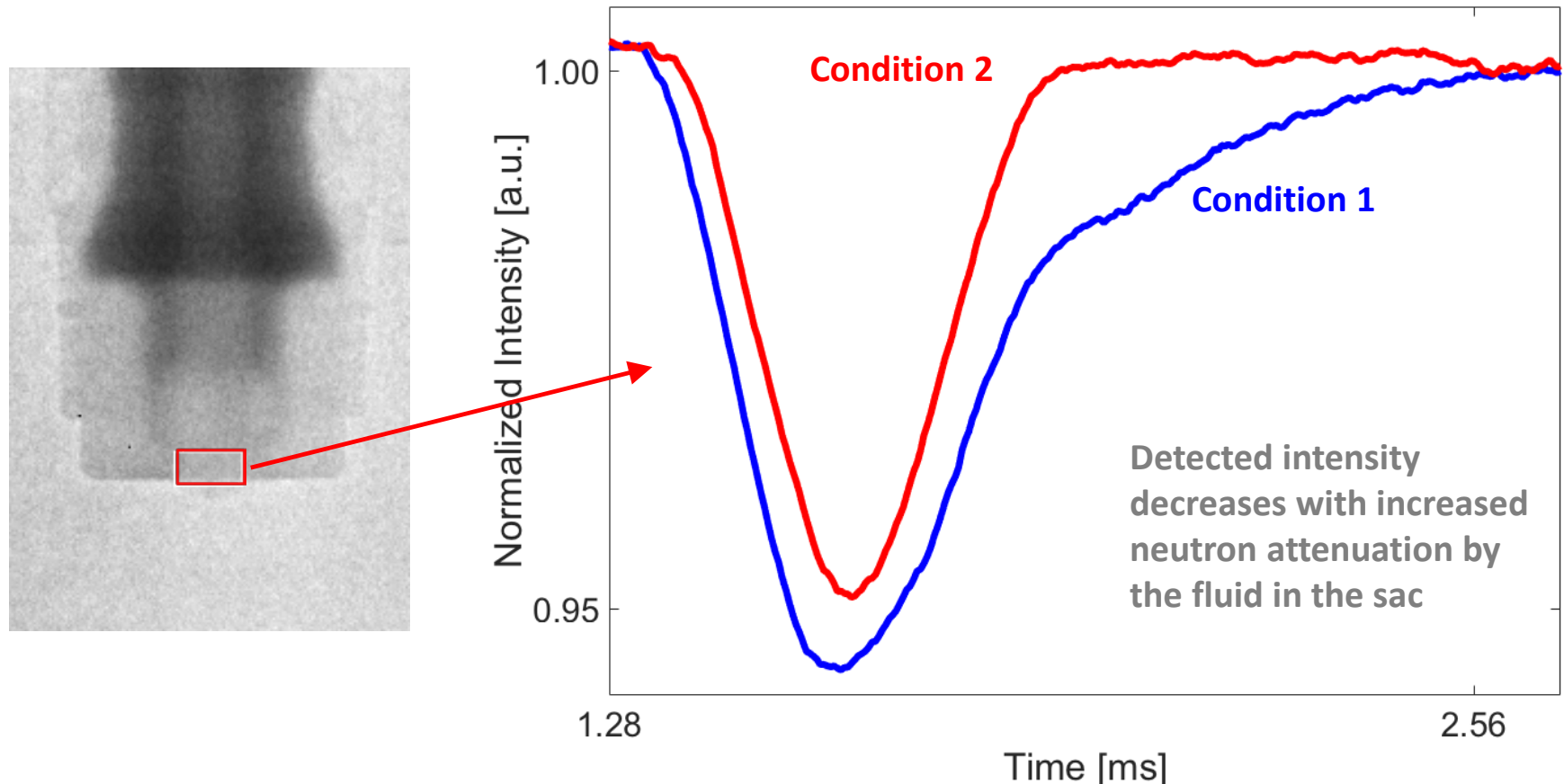
1.66 ms

1.79 ms

1.92 ms

More neutron attenuation by the fluid is measured in the sac in Condition 1 (flash), and more in the spray in Condition 2 (non-flash).

Technical Accomplishments: Sac emptying rates differ with condition



Condition 1 (Flash): More neutron attenuation by the fluid is measured, and the sac takes longer to empty.

Condition 2 (Non-Flash): Less neutron attenuation by the fluid is measured, and the sac empties very quickly.

Responses to Previous Year Reviewers' Comments

- New project
- Not reviewed last year

Collaborations

Boston University – Developing computational models of cavitation in fuel injectors and small scale experiments of idealized fuel injector



Oak Ridge National Laboratory – Experimental data of cavitation in a real fuel injector through imaging at operating conditions using the ORNL HFIR



Remaining Challenges and Barriers

Large parameter ratios between phases makes achieving numerical and interfacial stability with physical values challenging in small scale modeling.

Resolution of HFIR images limits details that can be seen in real fuel injector.

We need accurate computation of Eulerian flow to get local pressure threshold of cavitation.

We need experiments with controlled nuclei size and concentration to understand causes of cavitation onset.

We need to quantify spatial distributions of type of cavitation:

- High-speed imaging
- Passive Cavitation Mapping (PCM)

Proposed Future Work

On Going

- Small scale experiments at various operating conditions to understand the conditions that initiate cavitation
- Implementation and testing of RANS cavitation model based on OpenFOAM and built-in submodels
- Continued development and validation of small scale cavitation model

Planned

- Second imaging campaign with the ORNL HFIR. A proposal has been submitted for beam time on the ORNL HFIR to image the fuel injector under operating conditions that are expected to induce cavitation
- Joint BU-ORNL acoustic experiments on ORNL fuel injector assembly (not in HFIR beam) to use BU laser vibrometer to measure acoustics to directly compare with neutron imaging (May 2017)
- Control cavitation by controlling nucleation for purposes of mitigating cavitation damage and producing desired nozzle exit spray characteristics

Summary

Initial SPH model development included the addition of multiphase physics to an existing free surface flow SPH code and initial validation of bubble dynamics.

- Considering bubble dynamics under realistic densities, bubble shape and equilibrium
- Implementing model in conical nozzle for comparison to experimental data
- Developing RANS CFD model for larger nozzle simulation

Baseline experimental system developed which demonstrates capability of providing canonical data for comparison with computational results.

Successful imaging campaign of a real fuel injector using the HFIR at ORNL

- 96 continuous hours of experiment
- 2 spray conditions using cyclopentane – flash and non-flash
- Initial data analysis shows intriguing results between two injection conditions
- ORNL CT scan data of fuel injector transferred to BU for solid-modeling analysis

Acknowledgement

- This material is based upon work supported by the Department of Energy, Office of Energy Efficiency and Renewable Energy (EERE) and the Department of Defense, Tank and Automotive Research, Development, and Engineering Center (TARDEC), under Award Number DE-EE0007332.”

Technical Backup Slides

SPH Formulation

Smoothing function is used to approximate the governing equations

$$A_s(\bar{x}) = \int A(\bar{x}') W(\bar{x} - \bar{x}', h) d\bar{x}'$$

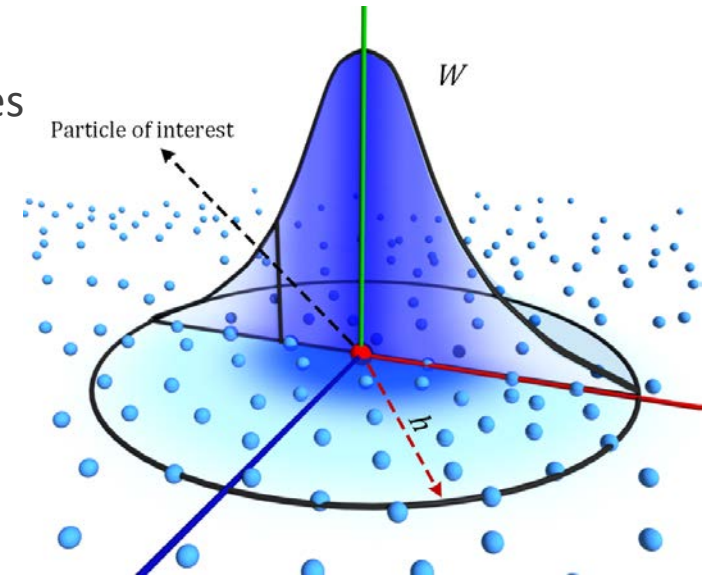
Simulation domain is divided into discrete particles

$$A_s(\bar{x}) = \sum_i \frac{A_i}{n_i} W(\bar{r}_{ij}, h)$$

Momentum Conservation (Navier-Stokes)

$$\rho \frac{D\bar{v}}{Dt} = -\nabla P + \mu \nabla^2 \bar{v} + \rho \bar{g}$$

$$\frac{D\bar{v}_i}{Dt} = -\frac{1}{m_i} \sum_{j \in \text{fluid} + \text{solid}} \left(\frac{P_j}{n_j^2} + \frac{P_i}{n_i^2} \right) \nabla_i W(\bar{r}_{ij}, h) + \frac{1}{m_i} \sum_{j \in \text{fluid} + \text{solid}} \frac{(\mu_i + \mu_j) \bar{v}_{ij}}{n_i n_j} \frac{\bar{r}_{ij}}{\bar{r}_{ij}^2} \cdot \nabla_i W(\bar{r}_{ij}, h) + F_i^{\text{ext}}$$



Sampath, Ramprasad, et al. (2016)

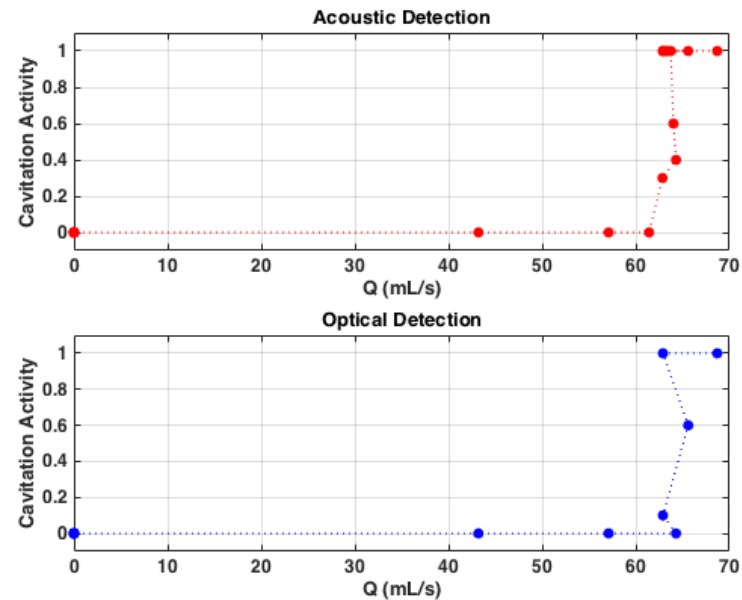
Code validation from experimental results

Experiments tell us:

1. Onset threshold
2. Nuclei type, size, concentration
3. 'Sheet' threshold
4. Inertial cavitation at onset, sheet cavitation as flow increases

Computation must:

1. Incorporate a cavitation inception criterion which agrees with experimental onset
2. Exhibit same nuclei parameter variation
3. Transition to coherent sheet structures at same flow rates
4. Yield inertial collapses for onset parameters

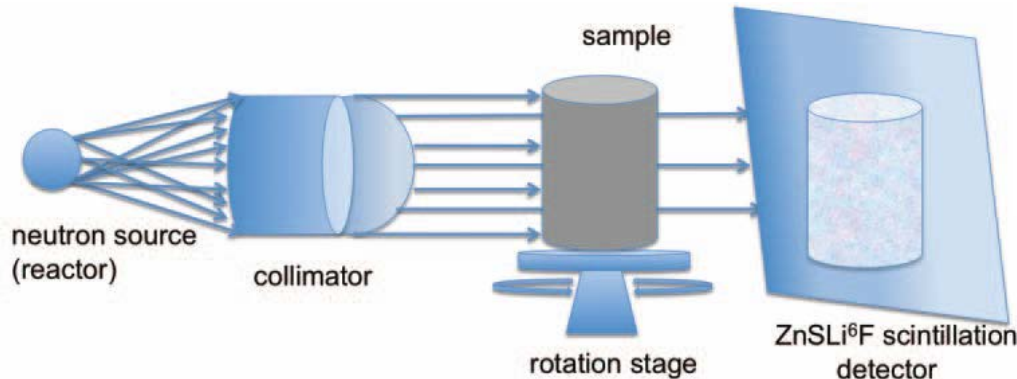


Neutrons can penetrate metals while still strongly interacting with light elements

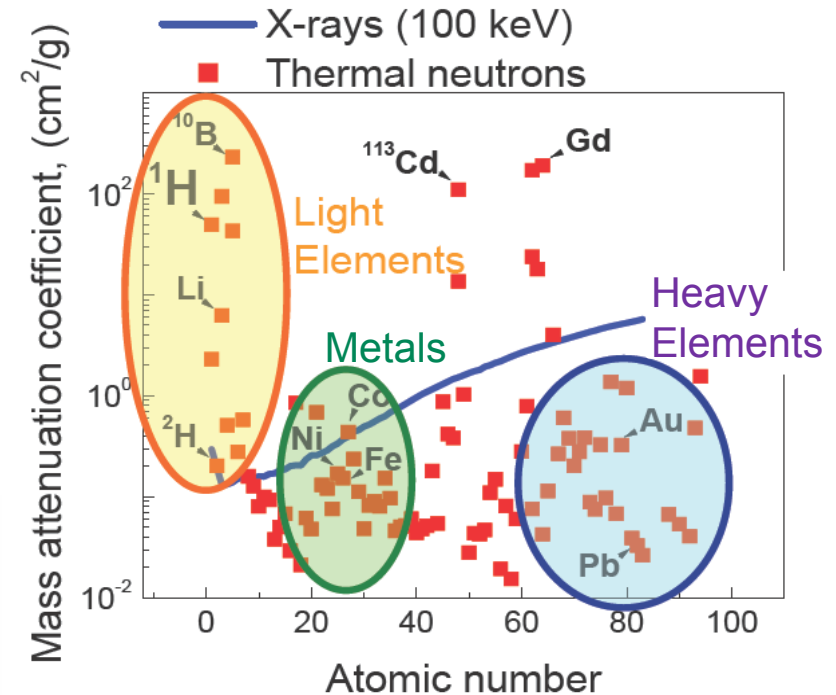
Neutrons are heavily attenuated by some light elements (^1H , ^{10}B , et)

- Can penetrate metals with minimal interactions
- Highly sensitive to water and hydrocarbons/fuel
- Image is based on absence of neutrons

X-ray absorption increases for heavy/dense elements



Attenuation Coefficient Reference: N. Kardjilov's presentation at IAN2006
http://neutrons.ornl.gov/workshops/ian2006/MO1/IAN2006oct_Kardjilov_02.pdf



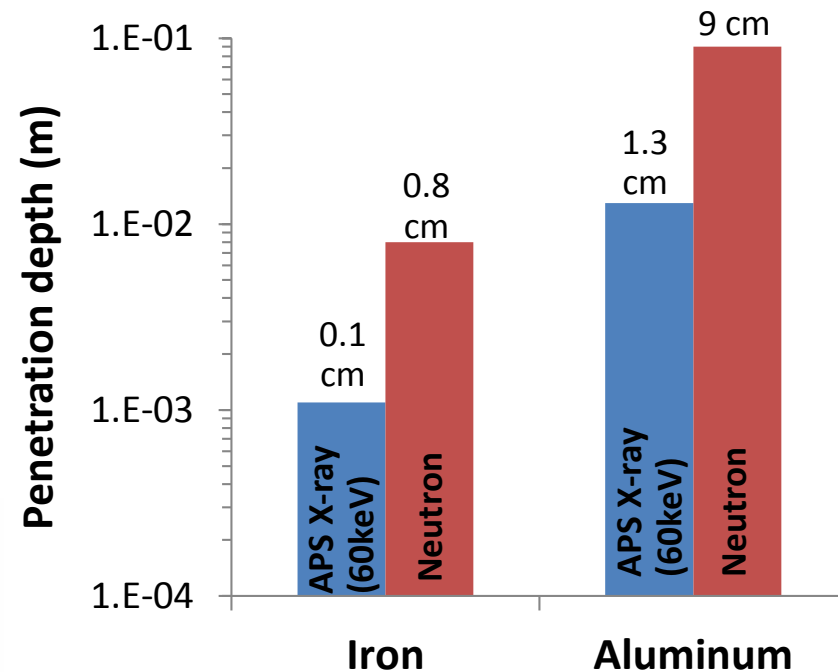
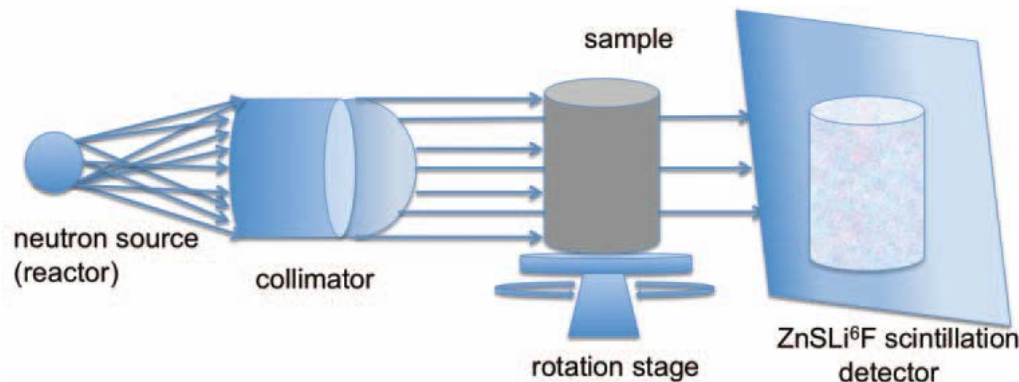
Neutron imaging is a complementary analytical tool

Neutrons can penetrate metals while still strongly interacting with light elements

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http://neutrons.ornl.gov/workshops/ian2006/MO1/IAN2006oct_Kardjilov_02.pdf

Neutron Penetration depth : R. Pynn, "Neutron scattering: a primer." *Los Alamos Science* 19 (1990): 1-31.
APS X-ray penetration depth: C. Powell, personal communication.

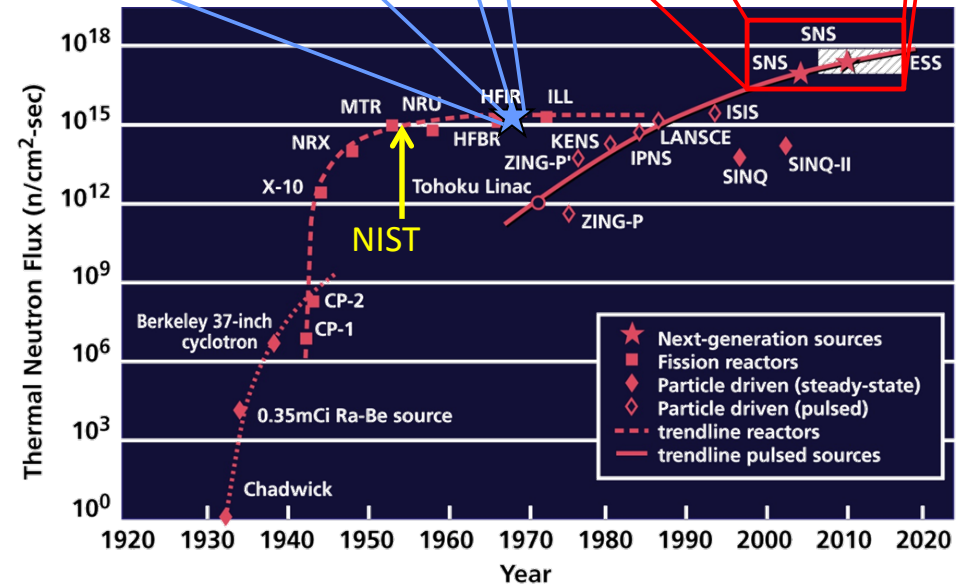
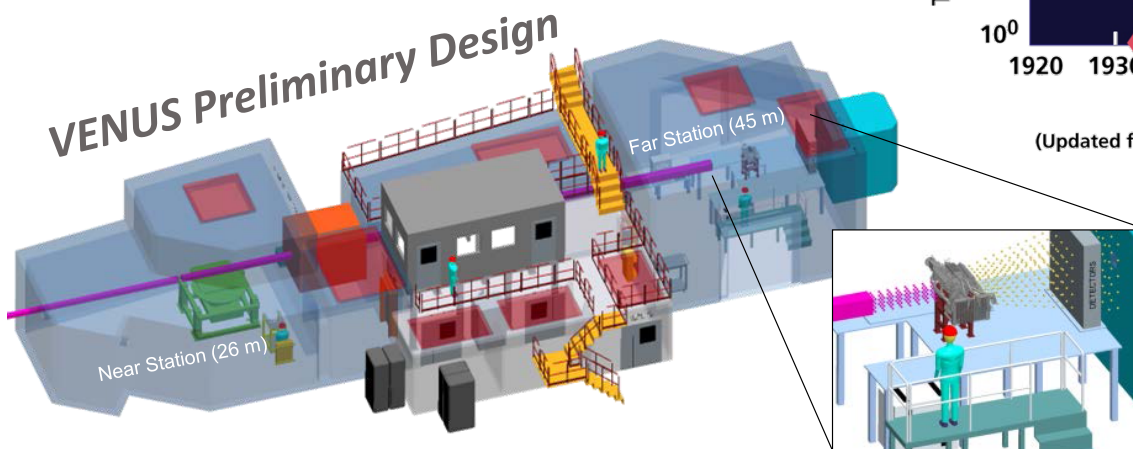
Neutrons at ORNL

High Flux Isotope Reactor (HFIR)

- Steady (i.e., non-pulsed) neutron source; “white” beam
- Imaging beam line accessible through user program

Spallation Neutron Source (SNS)

- Most intense pulsed neutron beam in the world; energy selective
- EERE promised \$12M to VENUS imaging beamline; manufacturing
 - 39 months to build



(Updated from *Neutron Scattering*, K. Skold and D. L. Price: eds., Academic Press, 1986)

Estimated Beam Characteristics

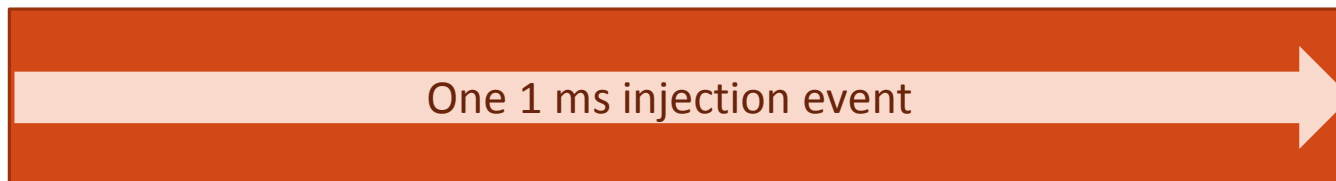
| Resolution | 20 μm | 50 μm | 200 μm |
|-----------------------------|------------------|------------------|-------------------|
| Max Field of View (cm x cm) | 2 x 2 | 20 x 20 | 30x30 |

Stroboscopic technique images internal fluid with ~ 1 ms injection, $20\ \mu\text{s}$ resolution

Sensor is Micro Channel Plate (MCP) detector, which allows very tight time bins

Injection timing for composite image:

- 0.4 - 1 ms injection with $20\ \mu\text{s}$ resolution
- Targeting ~ 30 s of neutron exposure for each $20\ \mu\text{s}$ frame
- Time-lapse imaging by aggregating stroboscopic sampling over $\sim 10^6$ injections

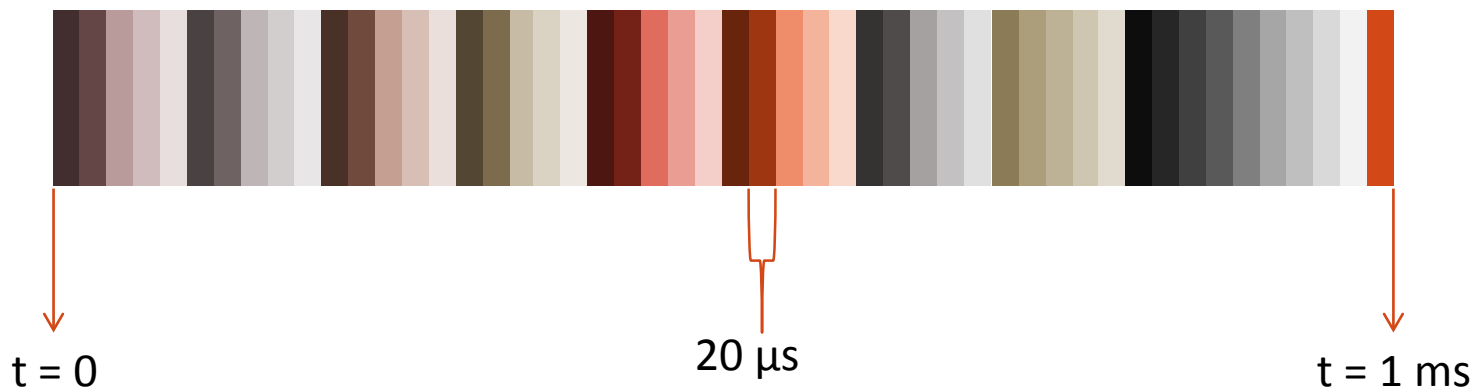


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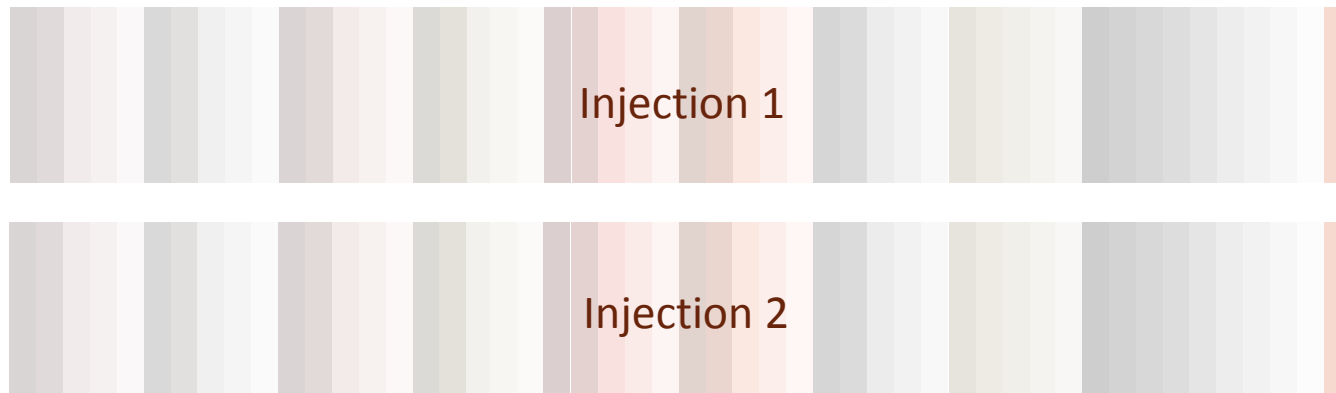


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